

# The Characterization of Trough Cross-Bedded Sedimentary Structures and Palaeoflow Direction from Down- Hole FMI Images

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# *Structure*

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- ◆ **Conventional FMI Analysis for Palaeoflow Direction**
- ◆ **Problems with the Conventional Technique**
- ◆ **A New Model for FMI Intersection Curves**
- ◆ **Application to FMI data**
- ◆ **Summary**

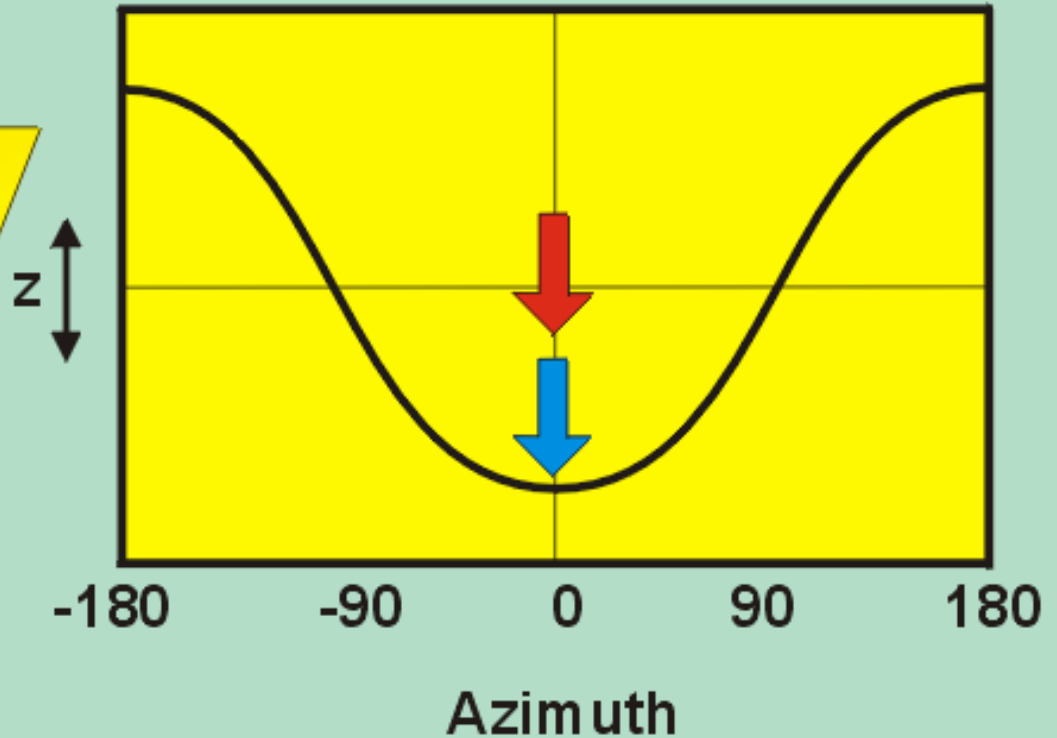
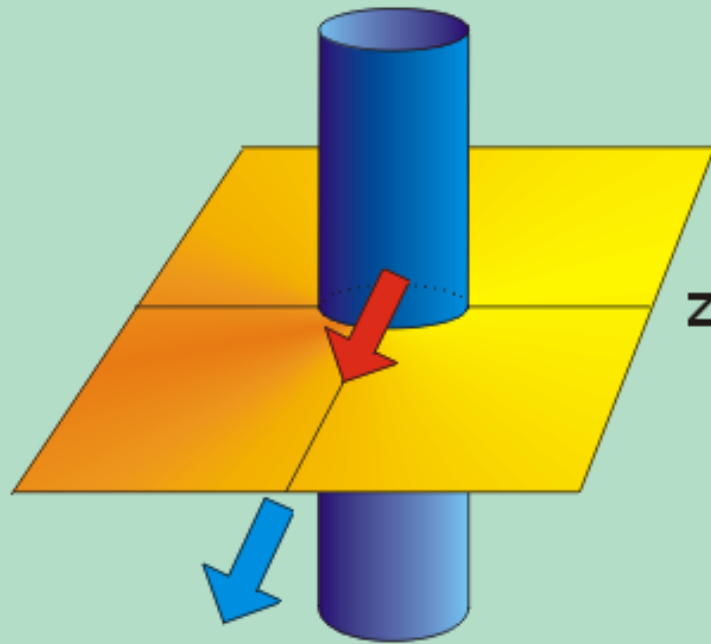


# *Conventional FMI Analysis*

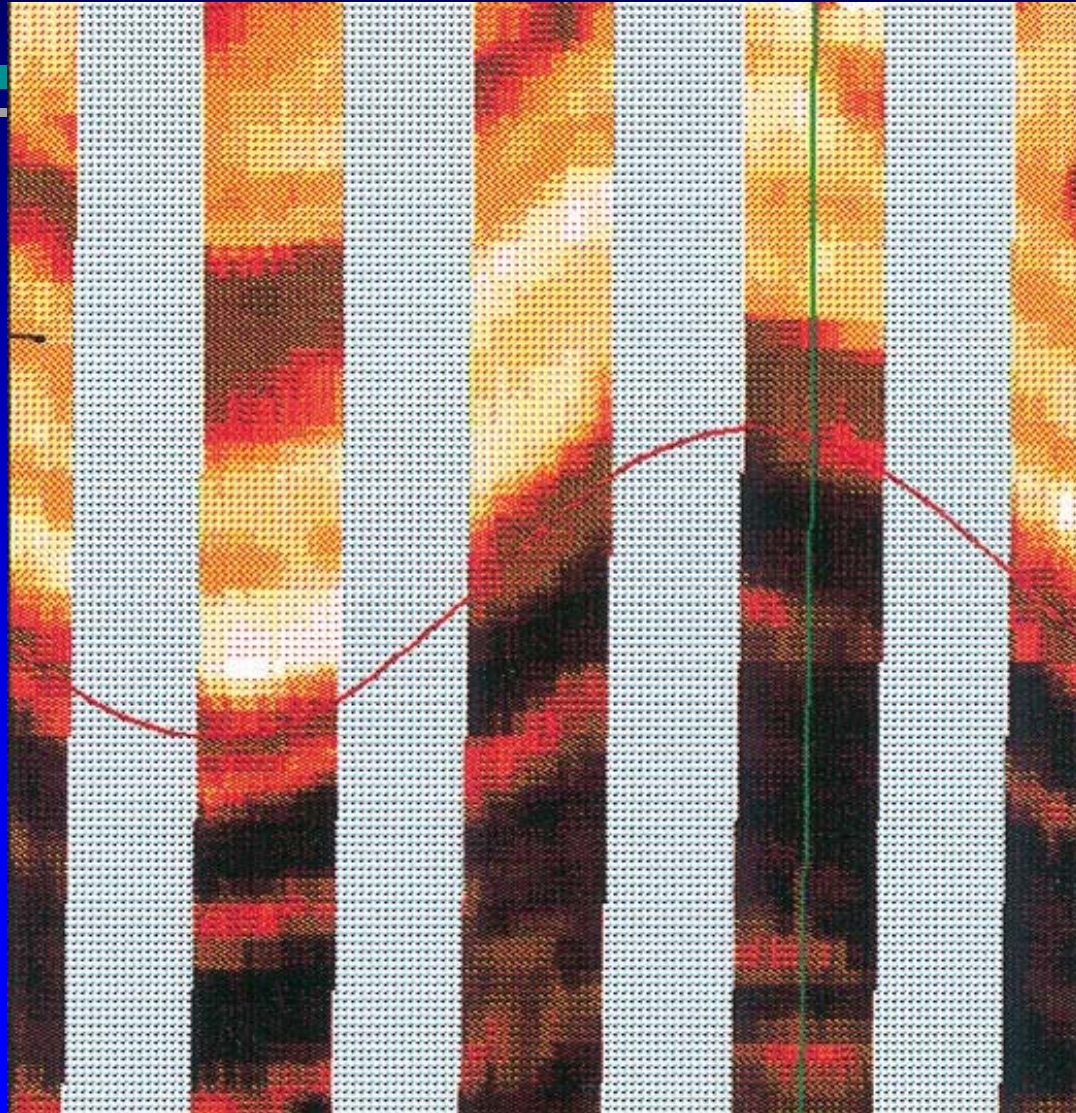
- ◆ **FMI is an electrical technique used in boreholes to image bedding and fractures around the perimeter of the borehole**
- ◆ **FMI images of planar bedforms cut the borehole with sinusoidal intersection curves**
- ◆ **The amplitude of the curves indicate the dip of the bedding**
- ◆ **The position of the minimum indicates the azimuth of the maximum dip (palaeoflow direction)**

# FMI Intersection Curves - Plane Bedding

## Plane Bedding



# *FMI Intersection Curves - Data*





# *Problems with Conventional FMI Analysis*

- ◆ In many cases the bedding is **NOT PLANAR**
- ◆ Trough cross-bedded structures produce intersection curves that look similar to true sinusoids, but are significantly different
- ◆ This gives **large errors in dip and azimuth**
- ◆ The problem is recognised and conventionally accounted for by averaging the results from many intersection curves
- ◆ Then hoping the errors cancel out!!!

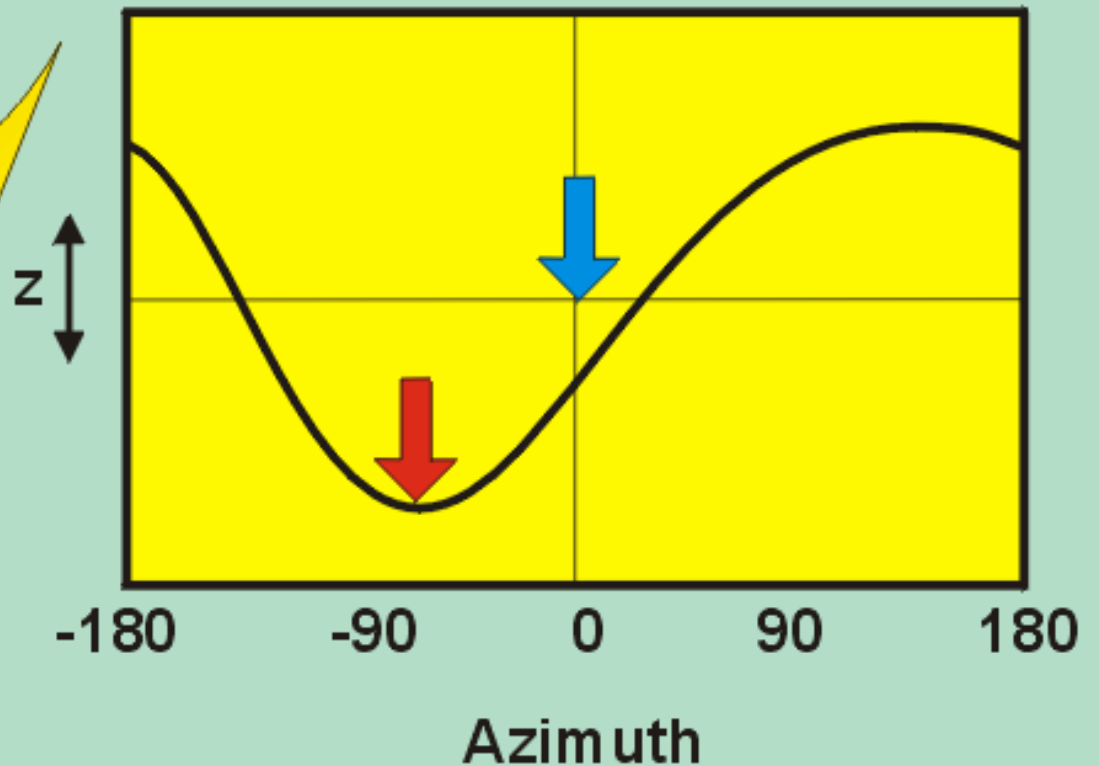
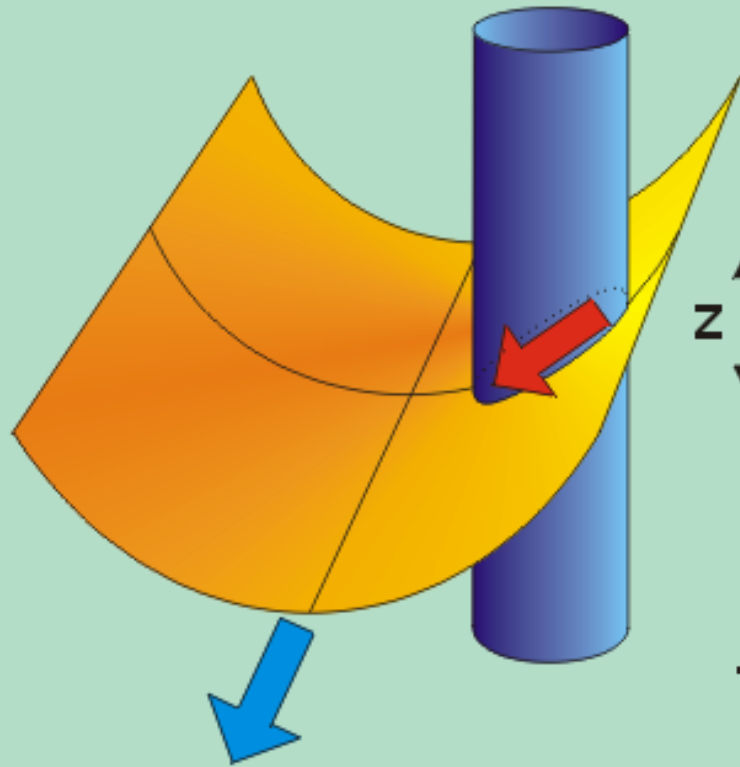


# *Conventional FMI Analysis*

- ◆ **They don't!**
- ◆ **The resulting data loses its vertical resolution (by about 50 times)**

# *FMI Intersection Curves - Trough Cross-Bedding*

## Trough Bedding







# ***Errors in Conventional FMI Analysis***

**There is no *a priori* knowledge of where the borehole intersects the trough**

- ◆ **If the borehole intersects the axis of the trough, the curve is similar to the plane case**
- ◆ **If the borehole does not intersect the axis of the trough, the side walls have the following effects:**
  - ◆ **The dip will be overestimated by as much as  $+40^\circ$**
  - ◆ **The azimuth will be in error by as much as  $\pm 90^\circ$**



# *Conventional Model*

- ◆ **Based on equations for the intersection of a circular borehole with a plane**
- ◆ **Parameters provided by the model are:**
  - ✎ **Azimuth,  $\phi$**
  - ✎ **Dip,  $\theta$**
- ◆ **Blindly applied to all data leads to errors in non-plane bedded systems**



# *New Model*

- ◆ **Based on equations for the intersection of a circular borehole with a hemi-circular trough**
- ◆ **Parameters provided by the model are:**
  - ✎ **Azimuth,  $\phi$**
  - ✎ **Dip,  $\theta$**
  - ✎ **Ratio of trough radius to borehole radius,  $d$**
  - ✎ **Ratio of offset distance to borehole radius,  $b$**
- ◆ **Blindly applied to all data does not lead to errors in plane or non-plane bedded systems**



# *New Model Equation*

**In its most general form the intersection equation is:**

$$z = \frac{1}{\cos \theta} \left[ \sin \theta \cos (\alpha - \varphi) + \sqrt{d^2 - (\sin (\alpha - \varphi) - b)^2} \right]$$

*$\theta = \text{Dip}$*

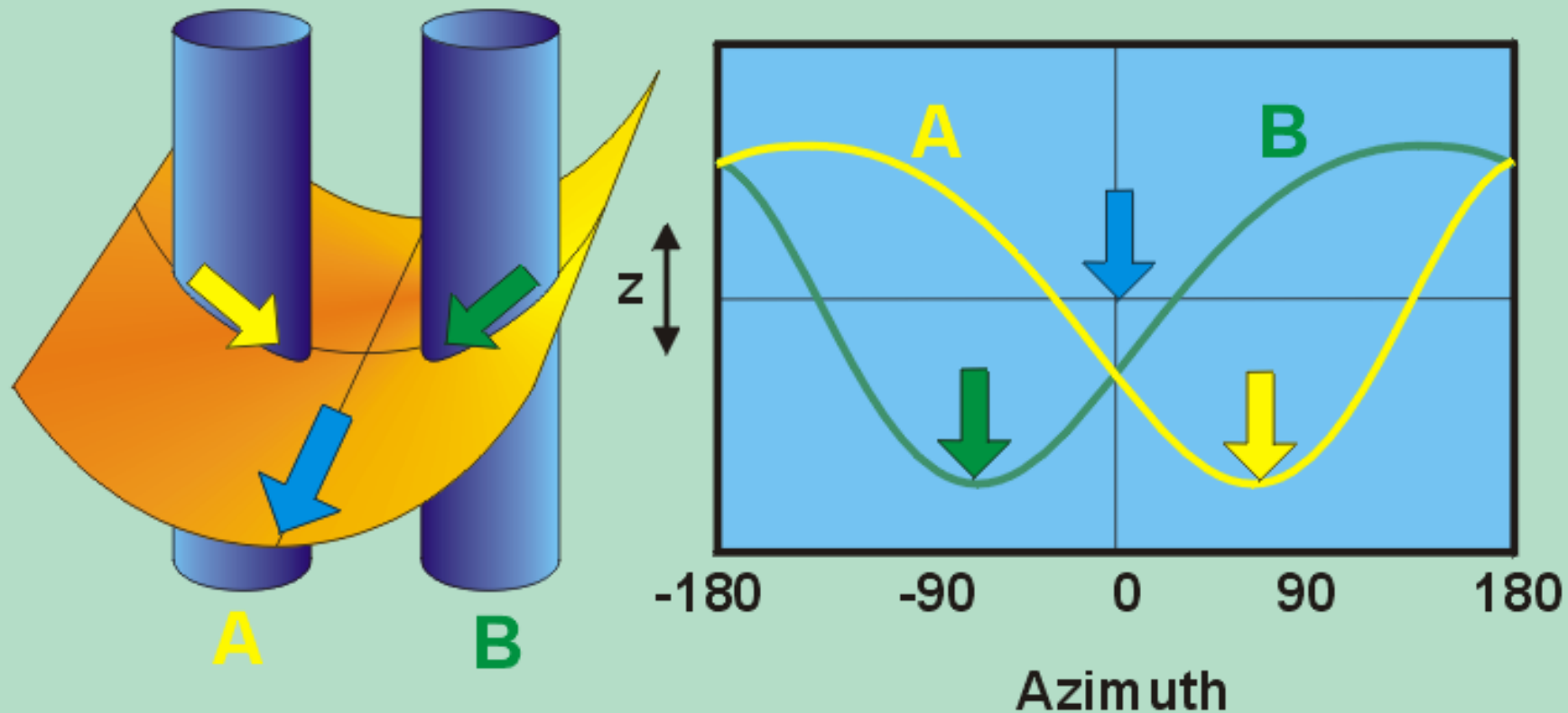
*$d = \text{Ratio of trough radius to borehole radius}$*

*$b = \text{Ratio of offset distance to borehole radius}$*

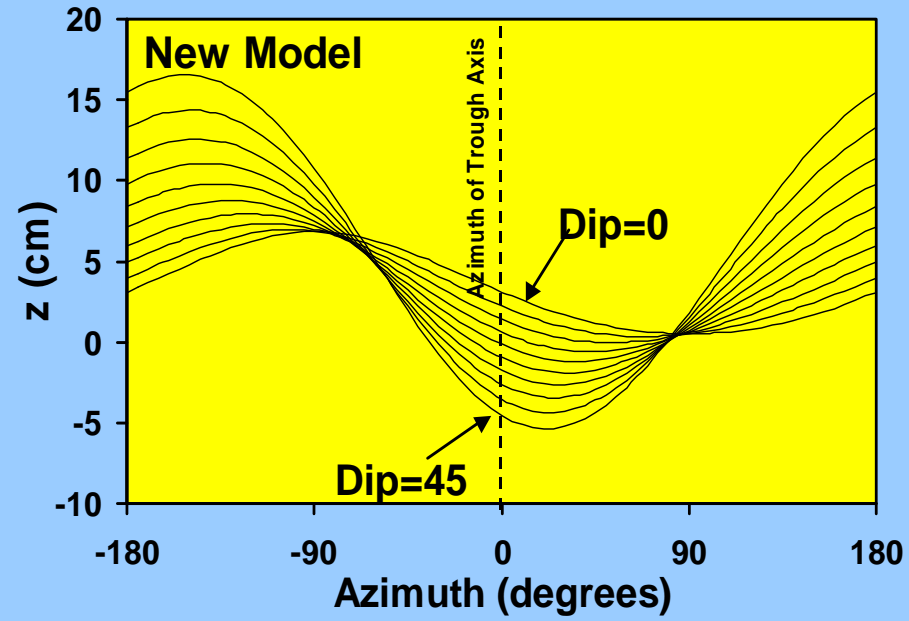
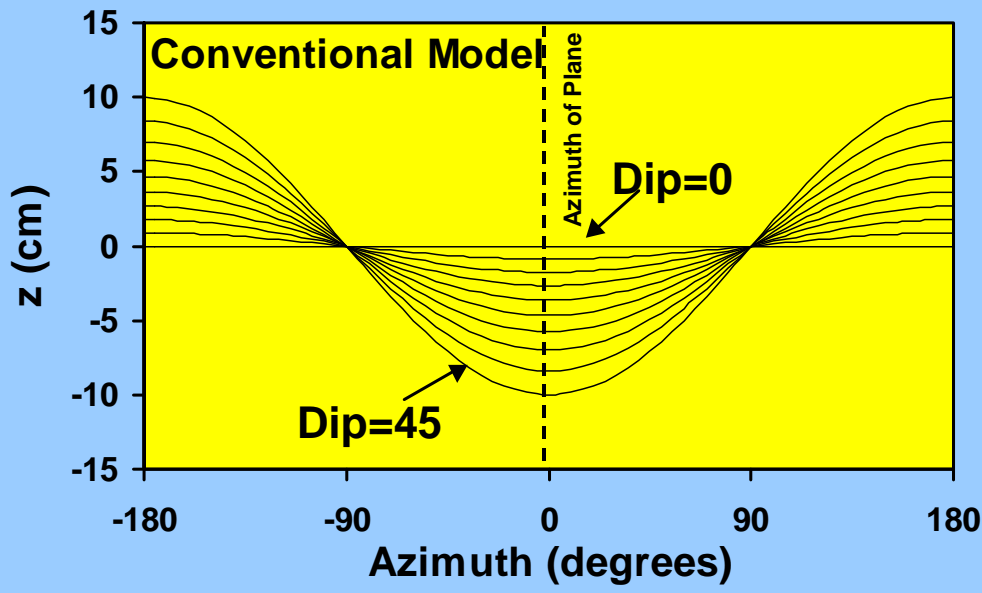
*Azimuth,  $\phi$  is derived from  $\varphi$  and  $\alpha$  by symmetry*

# *Derivation of Corrected Azimuth*

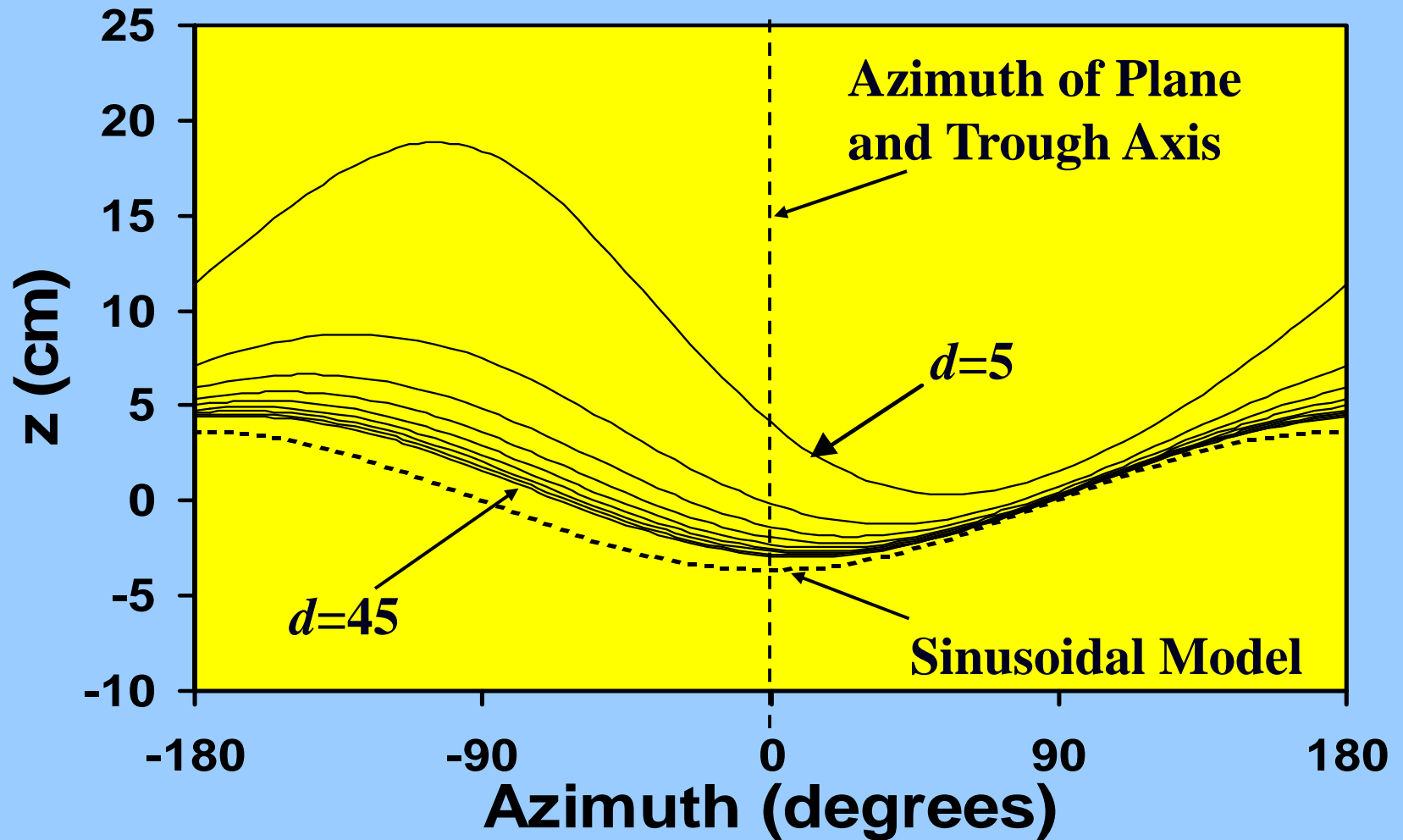
## Derivation of Corrected Azimuth



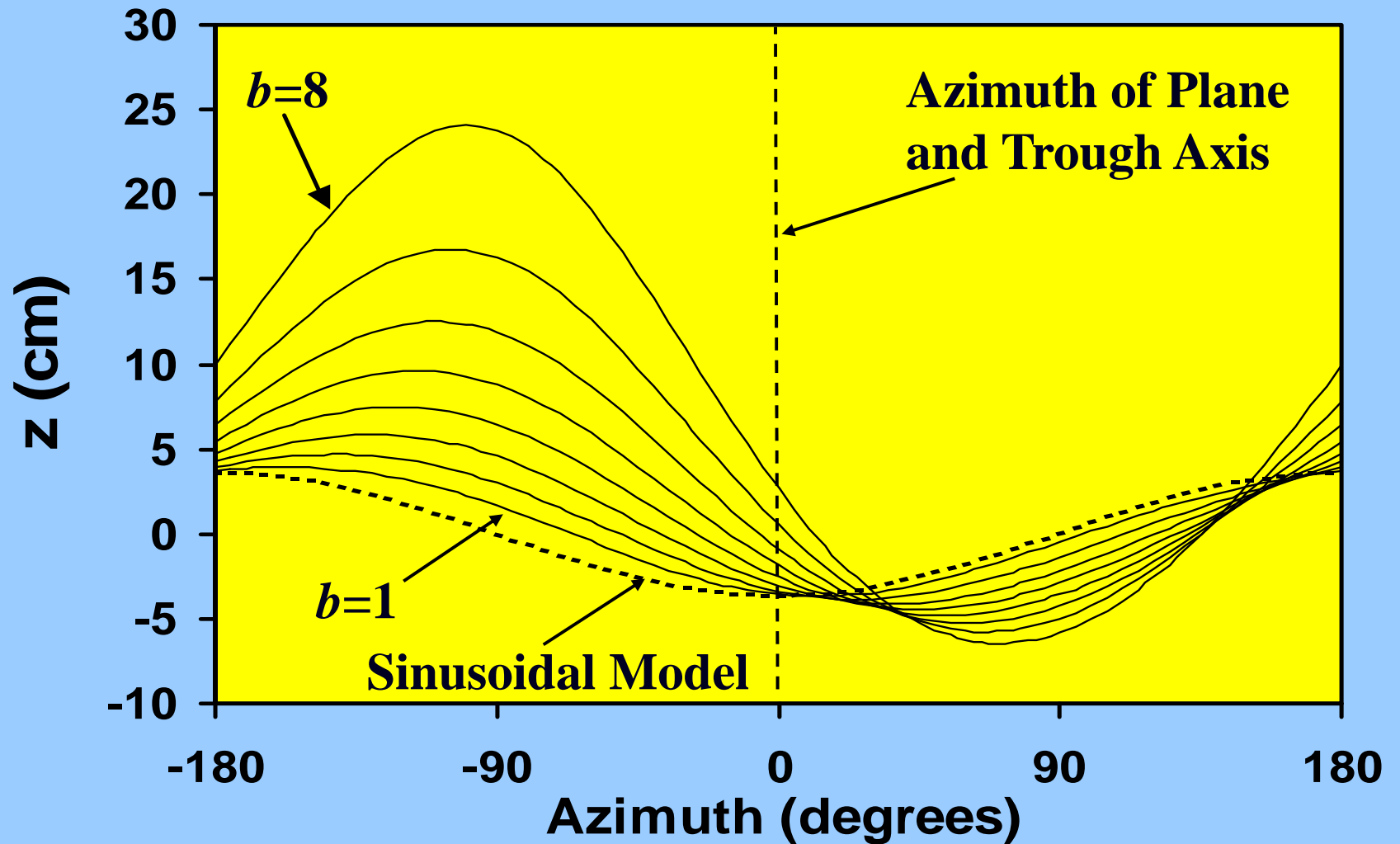
# FMI Intersection Curves



# *FMI Intersection Curves - Varying $d$*



# *FMI Intersection Curves - Varying $b$*







# *Testing the New Model*

- ◆ **55% Coverage FMI data**
- ◆ **39 intersection curves**
- ◆ **50 m of log**
- ◆ **Mixed trough and plane bedding**
- ◆ **Curves picked, digitised and fitted to conventional and new models**
- ◆ **Dip, azimuth,  $d$ , and  $b$  derived for each bed**
- ◆ **Statistical tests carried out to determine fit (Durbin-Watson autocorrelation)**



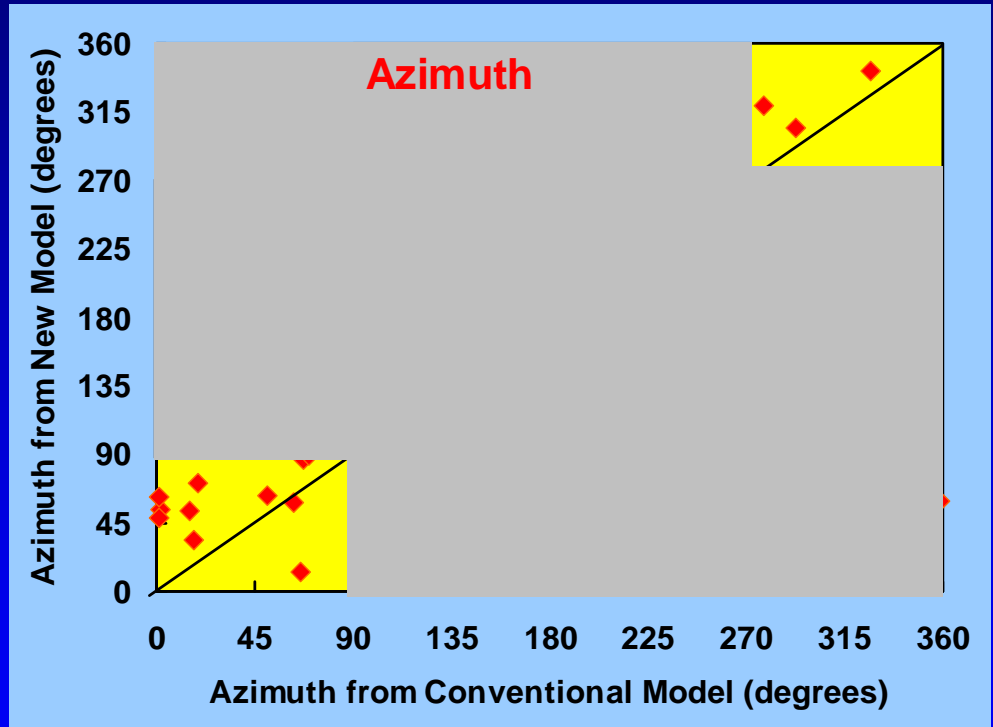
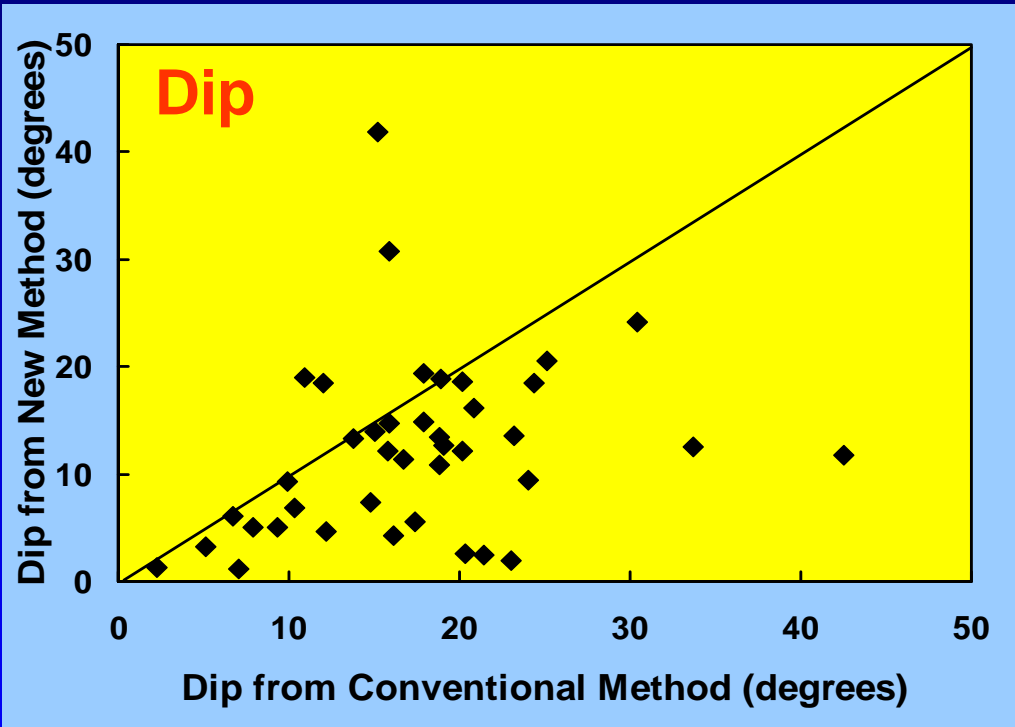
# *Testing Results I*

- ◆ The new model fitted the data better than the conventional model in the majority of cases

Test	Conventional	New
Sum of Squares	35.4	19.81
Absolute Deviation	0.021	0.015
Adjusted R <sup>2</sup>	96.4%	97.9%
Durbin-Watson (<0.8)	0.6631	1.050

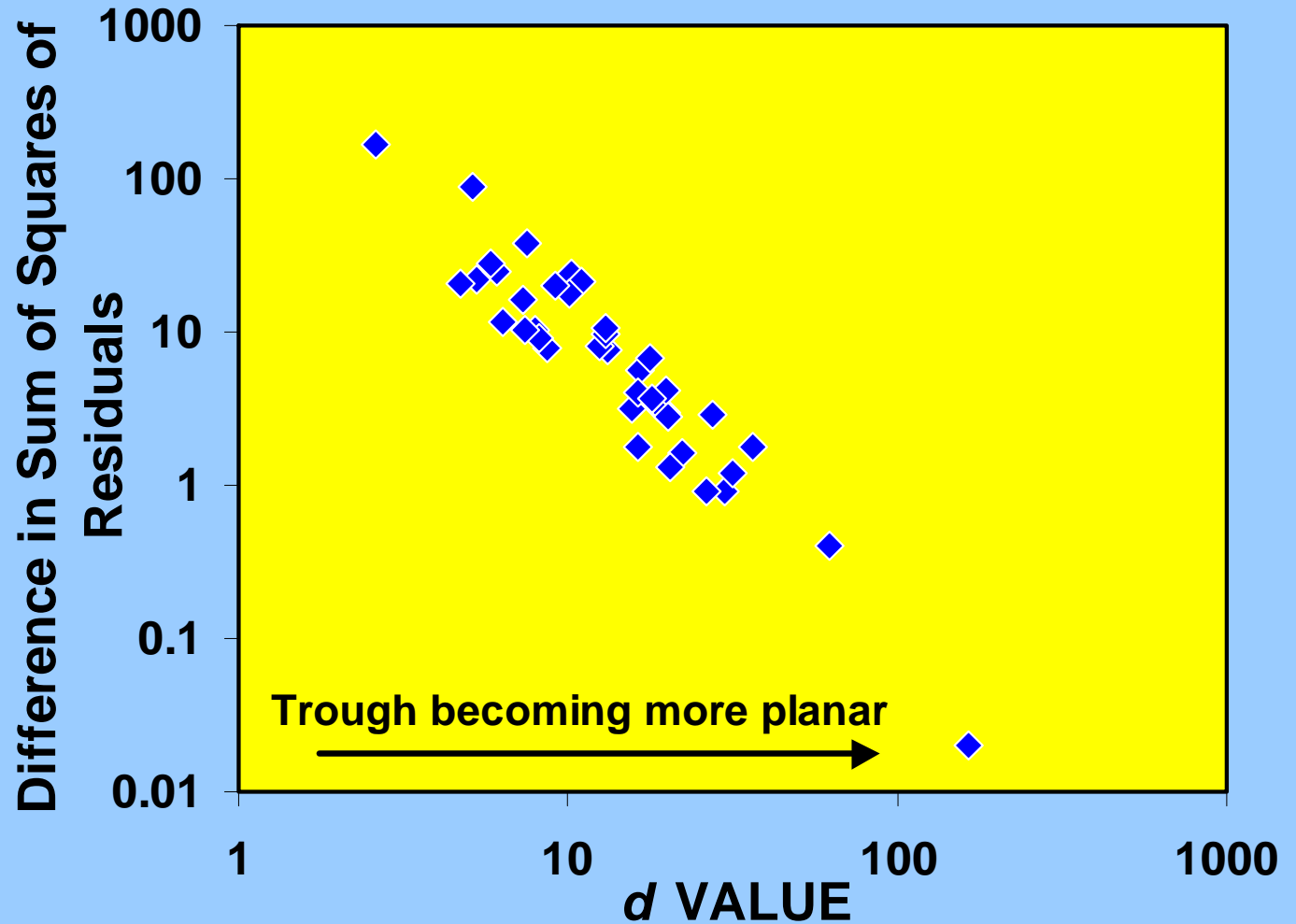
Mean values for all 39 curves

# Comparison of Two Methods - Dip and Azimuth



# Testing Results II

The difference in the two techniques becomes greater for acute troughs





# *Summary I*

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- ◆ **The conventional method for analysing FMI intersection curves often leads to large errors and low vertical resolutions in trough-bedded systems**
- ◆ **We have produced a new method for analysing FMI intersection curves that can be used to analyse plane and trough-bedded systems accurately with high resolution**



# *Summary II*

- ◆ **The conventional method provides data on mean dip and mean azimuth for sets of curves spanning a significant vertical interval**
- ◆ **The new method provides highly accurate values of dip, azimuth, trough radius and offset for individual structures**
- ◆ **This allows them to be mapped uniquely in the sub-surface**



# *Acknowledgements*

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